## Reply by Author to A. H. Flax

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A S remarked by Flax, the expressions derived by the author<sup>1</sup> for second-order sensitivities are limited to stiffness modifications for the conservative case. This is a consequence of the perturbation equation (3)<sup>1</sup>

$$(\lambda A + B)\underline{x} = \epsilon Q\underline{x}$$

where Q is treated throughout as a constant perturbation matrix and cannot subsequently be treated as a function of  $\lambda$ .

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The extension of the analysis provided by Flax shows that for mass modifications an additional term enters the second-order perturbation. This would be of considerable significance if the second-order sensitivities were to be used in the synthesis of modified systems. The original paper concerned itself specifically with the dangers of neglecting second-order sensitivities in system synthesis. In this respect, the work of Flax supports this, particularly his Eq. (8). A fuller treatment of this and similar problems may be found in Lancaster.<sup>2</sup>

Recent work by Tomita and Frohrib<sup>3</sup> may lead to extrapolations similar to those implied by Vanhonacker,<sup>4</sup> where second- and higher-order sensitivities are neglected in predicting effects due to design changes.

## References

<sup>1</sup>Brandon, J. A., "Derivation and Significance of Second-Order Modal Design Sensitivities," *AIAA Journal*, Vol. 22, May 1984, pp. 723-724.

<sup>2</sup>Lancaster, P., *Lambda Matrices and Vibrating Systems*, Pergamon, Press, New York, 1966.

<sup>3</sup>Tomita, K. and Frohrib, D. A., "Sensitivity Functions as Predictors of the Influence of Design Parameters on Frequency Response Properties." ASME Paper 83-DET-97, 1983.

Response Properties," ASME Paper 83-DET-97, 1983.

<sup>4</sup>Vanhonacker, P., "An Introduction to Sensitivity Analysis," Sixth Modal Analysis Seminar, University of Leuven, Sept. 1981.

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